## Zamac Hammer-Screw" Nail Anchor

## PRODUCT DESCRIPTION

The Zamac Hammer-Screw is a unique, one-step nail drive anchor featuring a Phillips type head and a screw thread for use in concrete, block, brick or stone. It is available in 1/4" diameter and lengths ranging from $3 / 4$ " to 3 ". With a body formed from corrosion resistant Zamac alloy and a zinc plated carbon steel or Perma-Sealmm coated drive screw, this anchor has been developed as an improvement over standard nailin anchors.
The Zamac Hammer-Screw has been designed to provide a removable anchor with higher tension load capacities compared with traditional nailin when installed in concrete. The anchor is not recommended for overhead, life-sfety or sustained tensile loading applications unless special considerations are given to the allowable loads.
(see performance data section).

## GENERAL APPLICATIONS AND ITSES

- Brick Ties and Masonry Anchorage
- Electrical Fixtures
- Signage
- Drywall track
- Maintenance
- Surveillance equiptment


## FEATURES AND BENEFITS

+ General purpose anchoring
+ Installs in a variety of base materials
+ Removable anchor when screw is backed out with a Phillips head driver


## APPROVALS AND LISTINGS

Federal GSA Specification Meets the proof load requirements of FF-S-325C, Group V, Type 2, Class 3, (superseded) and CID A-A 1925A, Type 1

## GUIDE SPECIFICATIONS

CSI Divisions: 03151-Concrete Anchoring, 04081-Masonry Anchorage and 05090-
Metal Fastenings. Nail Anchors shall be Zamac Hammer-Screw anchors as supplied by Powers Fasteners, Inc., Brewster, NY.

SECTION CONTENTS Page No.
General Information..................... 1
Installation and Material Specifications .. 1
Performance Data......................... 2
Design Criteria .............................. 3
Ordering Information ................... 4


Zamac Hammer-Screw

## ANCHOR MATERIALS

Zamac Alloy with Carbon Steel Drive Screw or Perma-Sealтм Coated Carbon Steel Drive Screw

## ANCHOR SIZE RANGE (TYP.)

$1 / 4^{\prime \prime} \times 3 / 4^{\prime \prime}$ to $1 / 4^{\prime \prime} \times 3^{\prime \prime}$ diameter

## SUITABLE BASE MATERIALS

Normal-weight Concrete
Hollow Concrete Masonry (CMU)
Brick Masonry
Stone

## INSTALLATION AND MATERIAL SPECIFICATIONS

## Installation Specifications

| Dimension | Anchor Diameter, $\boldsymbol{d}$ |
| :--- | :---: |
|  | $\mathbf{1 / 4 "}$ |
| ANSI Drill Bit Size, $d_{\text {bit }}$ (in.) | $1 / 4$ |
| Fixture Clearance Hole (in.) | $5 / 16$ |
| Head Height (in.) | $9 / 64$ |
| Head Width $d_{h d}$ (in.) | $35 / 64$ |

## Material Specifications

| Anchor <br> Component | Component Material |
| :--- | :---: |
|  | Mushroom Head |
| Drive Screw | Carbon Steel Screw |
| Anchor Body | AISI 1018 |
| Screw Plating | ASTM B 633, SC1, Type III (Fe/Zn 5) |
| Screw Coating | Perma-Seal Fluoropolymer |

## Installation Guidelines

Drill a hole into the base material to a depth of at least $1 / 4$ " deeper than the required embedment. The tolerances of the drill bit used should meet the requirements of ANSI Standard B212.15. Blow the hole clean of dust and other material.


Insert the anchor through the fixture. Drive the screw into the anchor body to expand it. Be sure the head is seated firmly against the fixture and that the anchor is at the proper embedment.


To remove - Press a Phillips screw driver firmly into the screw head and turn counterclockwise. Remove the screw from the anchor body, then pry out the fixture and anchor body simultaneously by working the claw of a hammer under the fixture


FASTENERS

## PERFORMANCE DATA

Ultimate Load Capacities for Zamac Hammer-Screw in Normal-Weight Concrete ${ }^{1,2}$

| Anchor Diameter <br> d in. (mm) | Minimum Embedment Depth $h_{v}$ in. (mm) | Minimum Concrete Compressive Strength ( $f_{c}^{\prime}$ ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2,000 psi (13.8 MPa) |  | 4,000 psi (27.6 MPa) |  | 6,000 psi (41.4 MPa) |  |
|  |  | Tension lbs. (kN) | Shear lbs. (kN) | Tension lbs. (kN) | Shear lbs. (kN) | Tension lbs. (kN) | Shear lbs. (kN) |
| $\begin{gathered} 1 / 4 \\ (6.4) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} \hline 675 \\ (3.0) \end{gathered}$ | $\begin{aligned} & \hline 650 \\ & (2.9) \end{aligned}$ | $\begin{aligned} & \hline 850 \\ & (3.8) \end{aligned}$ | $\begin{gathered} \hline 880 \\ (4.0) \end{gathered}$ | $\begin{gathered} \hline 890 \\ (4.0) \end{gathered}$ | $\begin{aligned} & 880 \\ & (4.0) \end{aligned}$ |
|  | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{gathered} 790 \\ (3.6) \end{gathered}$ | $\begin{aligned} & 805 \\ & (3.6) \end{aligned}$ | $\begin{aligned} & 1,135 \\ & (5.1) \end{aligned}$ | $\begin{aligned} & 1,115 \\ & (5.0) \end{aligned}$ | $\begin{aligned} & 1,190 \\ & (5.4) \end{aligned}$ | $\begin{aligned} & 1,115 \\ & (5.0) \end{aligned}$ |
|  | $\begin{gathered} 7 / 8 \\ (22.2) \end{gathered}$ | $\begin{aligned} & 930 \\ & (4.2) \end{aligned}$ | $\begin{aligned} & \hline 990 \\ & (4.5) \end{aligned}$ | $\begin{aligned} & 1,205 \\ & (5.4) \end{aligned}$ | $\begin{aligned} & 1,230 \\ & (5.5) \end{aligned}$ | $\begin{aligned} & 1,250 \\ & (5.6) \end{aligned}$ | $\begin{aligned} & 1,230 \\ & (5.5) \end{aligned}$ |
|  | $\begin{gathered} 11 / 8 \\ (28.6) \end{gathered}$ | $\begin{aligned} & \hline 1,220 \\ & (5.5) \end{aligned}$ | $\begin{aligned} & \hline 1,365 \\ & (6.1) \end{aligned}$ | $\begin{aligned} & 1,350 \\ & (6.1) \end{aligned}$ | $\begin{aligned} & 1,470 \\ & (6.6) \end{aligned}$ | $\begin{aligned} & \hline 1,450 \\ & (6.5) \end{aligned}$ | $\begin{aligned} & \hline 1,470 \\ & (6.6) \end{aligned}$ |
|  | $\begin{array}{r} 13 / 8 \\ (34.9) \end{array}$ | $\begin{aligned} & 1,325 \\ & (6.0) \end{aligned}$ | $\begin{aligned} & 1,555 \\ & (7.0) \end{aligned}$ | $\begin{gathered} 1,450 \\ (6.5) \end{gathered}$ | $\begin{gathered} 1,645 \\ (7.4) \end{gathered}$ | $\begin{aligned} & 1,530 \\ & (6.9) \end{aligned}$ | $\begin{aligned} & \hline 1,645 \\ & (7.4) \end{aligned}$ |
|  | $\begin{array}{r} 13 / 4 \\ (44.5) \end{array}$ | $\begin{aligned} & 1,480 \\ & (6.7) \end{aligned}$ | $\begin{aligned} & 1,840 \\ & (8.3) \end{aligned}$ | $\begin{aligned} & 1,600 \\ & (7.2) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,910 \\ & (8.6) \end{aligned}$ | $\begin{aligned} & 1,660 \\ & (7.5) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,910 \\ & (8.6) \end{aligned}$ |
|  | $\begin{gathered} 17 / 8 \\ (47.6) \end{gathered}$ | $\begin{aligned} & 1,480 \\ & (6.7) \end{aligned}$ | $\begin{aligned} & 1,840 \\ & (8.3) \end{aligned}$ | $\begin{aligned} & 1,600 \\ & (7.2) \end{aligned}$ | $\begin{aligned} & 1,910 \\ & (8.6) \end{aligned}$ | $\begin{gathered} 1,660 \\ (7.5) \end{gathered}$ | $\begin{aligned} & 1,910 \\ & (8.6) \end{aligned}$ |

1. Tabulated load values are for anchors installed in concrete. Concrete compressive strength must be at the specified minimum at the time of installation
2. Ultimate load capacities must be reduced by a minimum safety factor of 4.0 or greater to determine allowable working load. Consideration of safety factors of 20 or higher may be necessary depending upon the application such as life safety, overhead and in sustained tensile loading applications.

Allowable Load Capacities for Zamac Hammer-Screw in Normal-Weight Concrete ${ }^{1,2,3}$

| Anchor Diameter <br> d <br> in. (mm) | $\qquad$ | Minimum Concrete Compressive Strength ( $f_{c}^{\prime}$ ) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 2,000 psi (13.8 MPa) |  | 4,000 psi (27.6 MPa) |  | 6,000 psi (41.4 MPa) |  |
|  |  | Tension lbs. (kN) | Shear lbs. (kN) | Tension lbs. (kN) | Shear lbs. (kN) | Tension lbs. (kN) | Shear lbs. (kN) |
| $\begin{gathered} 1 / 4 \\ (6.4) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} \hline 170 \\ (0.8) \end{gathered}$ | $\begin{aligned} & \hline 165 \\ & (0.7) \end{aligned}$ | $\begin{aligned} & \hline 215 \\ & (1.0) \end{aligned}$ | $\begin{gathered} \hline 220 \\ (1.0) \end{gathered}$ | $\begin{gathered} \hline 225 \\ (1.0) \end{gathered}$ | $\begin{gathered} \hline 220 \\ (1.0) \end{gathered}$ |
|  | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{aligned} & \hline 200 \\ & (0.9) \end{aligned}$ | $\begin{aligned} & 200 \\ & (0.9) \end{aligned}$ | $\begin{gathered} 285 \\ (1.3) \end{gathered}$ | $\begin{gathered} 280 \\ (1.3) \end{gathered}$ | $\begin{gathered} 300 \\ (1.4) \end{gathered}$ | $\begin{gathered} 280 \\ (1.3) \end{gathered}$ |
|  | $\begin{gathered} 7 / 8 \\ (22.2) \end{gathered}$ | $\begin{aligned} & 235 \\ & (1.1) \end{aligned}$ | $\begin{gathered} \hline 250 \\ (1.1) \end{gathered}$ | $\begin{aligned} & 300 \\ & (1.4) \end{aligned}$ | $\begin{gathered} 310 \\ (1.4) \end{gathered}$ | $\begin{gathered} 315 \\ (1.4) \end{gathered}$ | $\begin{gathered} 310 \\ (1.4) \end{gathered}$ |
|  | $\begin{gathered} 11 / 8 \\ (28.6) \end{gathered}$ | $\begin{gathered} \hline 305 \\ (1.4) \end{gathered}$ | $\begin{gathered} \hline 340 \\ (1.5) \end{gathered}$ | $\begin{gathered} \hline 340 \\ (1.5) \end{gathered}$ | $\begin{gathered} \hline 370 \\ (1.7) \end{gathered}$ | $\begin{gathered} \hline 365 \\ (1.6) \end{gathered}$ | $\begin{gathered} \hline 370 \\ (1.7) \end{gathered}$ |
|  | $\begin{array}{r} 13 / 8 \\ (34.9) \end{array}$ | $\begin{gathered} \hline 330 \\ (1.5) \end{gathered}$ | $\begin{gathered} \hline 390 \\ (1.8) \end{gathered}$ | $\begin{aligned} & \hline 365 \\ & (1.6) \end{aligned}$ | $\begin{gathered} \hline 410 \\ (1.8) \end{gathered}$ | $\begin{aligned} & \hline 385 \\ & (1.7) \end{aligned}$ | $\begin{gathered} \hline 410 \\ (1.8) \end{gathered}$ |
|  | $\begin{gathered} 13 / 4 \\ (44.5) \end{gathered}$ | $\begin{gathered} \hline 370 \\ (1.7) \end{gathered}$ | $\begin{aligned} & \hline 460 \\ & (2.1) \end{aligned}$ | $\begin{aligned} & \hline 400 \\ & (1.8) \end{aligned}$ | $\begin{aligned} & 480 \\ & (2.2) \end{aligned}$ | $\begin{gathered} \hline 415 \\ (1.9) \end{gathered}$ | $\begin{aligned} & 480 \\ & (2.2) \end{aligned}$ |
|  | $\begin{gathered} 17 / 8 \\ (47.6) \end{gathered}$ | $\begin{aligned} & \hline 370 \\ & (1.7) \end{aligned}$ | $\begin{aligned} & 460 \\ & (2.1) \end{aligned}$ | $\begin{aligned} & \hline 400 \\ & (1.8) \end{aligned}$ | $\begin{aligned} & 480 \\ & (2.2) \end{aligned}$ | $\begin{gathered} \hline 415 \\ (1.9) \end{gathered}$ | $\begin{aligned} & 480 \\ & (2.2) \end{aligned}$ |

[^0]
## PERFORMANCE DATA

Ultimate and Allowable Load Capacities for Zamac Hammer Screw in Hollow Concrete Masonry ${ }^{1,2,3}$

| Anchor Diameter$\begin{gathered} d \\ \text { in. } \\ (\mathrm{mm}) \end{gathered}$ | Minimum <br> Embedment <br> Depth <br> $h_{v}$ <br> in. <br> $(\mathrm{mm})$ | $\boldsymbol{f}_{\boldsymbol{m}}^{\prime} \geq \mathbf{1 , 5 0 0} \mathbf{~ p s i}(10.4 \mathrm{MPa})$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Ultimate Load |  | Allowable Load |  |
|  |  | $\begin{gathered} \text { Tension } \\ \text { lbs. } \\ \text { (kN) } \\ \hline \end{gathered}$ | Shear lbs. (kN) | Tension lbs. (kN) | Shear lbs. (kN) |
| $\begin{gathered} 1 / 4 \\ (6.4) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 420 \\ & (1.9) \end{aligned}$ | $\begin{aligned} & 1,160 \\ & (5.2) \end{aligned}$ | $\begin{gathered} 85 \\ (0.4) \\ \hline \end{gathered}$ | $\begin{array}{r} \hline 230 \\ (1.0) \\ \hline \end{array}$ |
|  | $\begin{array}{r} 3 / 4 \\ (19.1) \\ \hline \end{array}$ | $\begin{aligned} & \hline 825 \\ & (3.7) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,215 \\ & (5.5) \\ & \hline \end{aligned}$ | $\begin{gathered} 165 \\ (0.7) \end{gathered}$ | $\begin{aligned} & 245 \\ & (1.1) \end{aligned}$ |
|  | $\begin{gathered} 1 \\ (25.4) \\ \hline \end{gathered}$ | $\begin{aligned} & 1,000 \\ & (4.5) \end{aligned}$ | $\begin{aligned} & 1,265 \\ & (5.7) \end{aligned}$ | $\begin{array}{r} 200 \\ (0.9) \\ \hline \end{array}$ | $\begin{array}{r} \hline 255 \\ (1.1) \\ \hline \end{array}$ |
|  | $\begin{array}{r} 11 / 8 \\ (28.6) \\ \hline \end{array}$ | $\begin{aligned} & 1,090 \\ & (4.9) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,290 \\ & (5.8) \\ & \hline \end{aligned}$ | $\begin{array}{r} 220 \\ (1.0) \\ \hline \end{array}$ | $\begin{array}{r} 260 \\ (1.2) \\ \hline \end{array}$ |
|  | $\begin{array}{r} 13 / 8 \\ (34.9) \\ \hline \end{array}$ | $\begin{aligned} & 1,145 \\ & (5.2) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,345 \\ & (6.1) \\ & \hline \end{aligned}$ | $\begin{aligned} & 230 \\ & (1.0) \end{aligned}$ | $\begin{array}{r} \hline 270 \\ (1.2) \end{array}$ |
|  | $\begin{array}{r} 11 / 2 \\ (38.1) \\ \hline \end{array}$ | $\begin{aligned} & 1,145 \\ & (5.2) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,345 \\ & (6.1) \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline 230 \\ (1.0) \\ \hline \end{array}$ | $\begin{gathered} 270 \\ (1.2) \\ \hline \end{gathered}$ |

1. Tabulated load values are for anchors installed in minimum 6 -inch wide, Grade N , Type II, medium and normal-weight and lightweight concrete masonry units. Mortar must be Type N , S or M . Masonry compressive strength must be 1,500 psi minimum at the time of installation. Masonry cells may be grouted.
2. The tabulated values are for anchors installed at a minimum of 16 anchor diameters on center for 100 percent capacity. Spacing distances may be reduced to 8 anchor diameters on center provied the capacities are reduced by 50 percent. Linear interpolation may be used for intermediate spacing.
3. Allowable load capacities listed are calculated using and applied safety factor of 5.0. Consideration of safety factors of 20 or higher may be necessary depending upon the application such as life safety, and in sustained tensile loading applications.
Ultimate and Allowable Load Capacities for Zamac-Hammer Screw in Solid Clay Brick Masonry ${ }^{1,2.3}$

| Anchor Diameter <br> $d$ in. (mm) | $\qquad$ | $\boldsymbol{f}_{\boldsymbol{m}}^{\prime} \geq \mathbf{1 , 5 0 0} \mathbf{~ p s i}(10.4 \mathrm{MPa})$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Ultimate Load |  | Allowable Load |  |
|  |  | Tension lbs. (kN) | Shear lbs. (kN) | Tension lbs. (kN) | Shear lbs. (kN) |
| $\begin{gathered} 1 / 4 \\ (6.4) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \\ \hline \end{gathered}$ | $\begin{aligned} & 680 \\ & (3.1) \end{aligned}$ | $\begin{aligned} & 1,400 \\ & (6,3) \end{aligned}$ | $\begin{aligned} & 135 \\ & (0.6) \end{aligned}$ | $\begin{aligned} & \hline 280 \\ & (1.3) \end{aligned}$ |
|  | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{aligned} & \hline 930 \\ & (4.2) \end{aligned}$ | $\begin{aligned} & 1,600 \\ & (7.2) \end{aligned}$ | $\begin{gathered} \hline 185 \\ (0.8) \end{gathered}$ | $\begin{array}{r} \hline 320 \\ (1.4) \end{array}$ |
|  | $\begin{gathered} 1 \\ (25.4) \\ \hline \end{gathered}$ | $\begin{array}{r} 990 \\ (4.5) \end{array}$ | $\begin{aligned} & 1,600 \\ & (7.2) \\ & \hline \end{aligned}$ | $\begin{array}{r} 200 \\ (0.9) \\ \hline \end{array}$ | $\begin{array}{r} 320 \\ (1.4) \\ \hline \end{array}$ |
|  | $\begin{aligned} & 11 / 8 \\ & (28.6) \end{aligned}$ | $\begin{aligned} & 1,040 \\ & (4.7) \end{aligned}$ | $\begin{aligned} & 1,600 \\ & (7.2) \end{aligned}$ | $\begin{gathered} \hline 210 \\ (0.9) \end{gathered}$ | $\begin{aligned} & \hline 320 \\ & (1.4) \end{aligned}$ |
|  | $\begin{array}{r} 13 / 8 \\ (34.9) \\ \hline \end{array}$ | $\begin{aligned} & 1,150 \\ & (5.2) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,600 \\ & (7.2) \\ & \hline \end{aligned}$ | $\begin{array}{r} 230 \\ (1.0) \\ \hline \end{array}$ | $\begin{array}{r} 320 \\ (1.4) \\ \hline \end{array}$ |
|  | $\begin{array}{r} 11 / 2 \\ (38.1) \\ \hline \end{array}$ | $\begin{aligned} & 1,260 \\ & (5.7) \end{aligned}$ | $\begin{aligned} & 1,600 \\ & (7.2) \\ & \hline \end{aligned}$ | $\begin{array}{r} 250 \\ (1.1) \\ \hline \end{array}$ | $\begin{array}{r} 320 \\ (1.4) \\ \hline \end{array}$ |

1. Tabulated load values are for anchors installed in multiple wythe, minimum Grade SW, solid clay brick masonry walls conforming to ASTM C 62. Mortar must be minimum Type N. Masonry compressive strength must be at the specified minimum at the time of installation ( $f^{\prime} m \geq 1,500 \mathrm{psi}$ ).
2. The tabulated values are for anchors installed at a minimum of 16 anchor diameters on center for 100 percent capacity. Spacing distances may be reduced to 8 anchor diameters on center provied the capacities are reduced by 50 percent. Linear interpolation may be used for intermediate spacing
3. Allowable load capacities listed are calculated using and applied safety factor of 5.0. Consideration of safety factors of 20 or higher may be necessary depending upon the application such as life safety, and in sustained tensile loading applications.

## DESIGN CRITERIA (ALLOWABLE STRESS DESIGN)

## Combined Loading

For anchors loaded in both shear and tension, the combination of loads should be proportioned as follows:

$$
\left(\frac{N_{u}}{N_{n}}\right)+\left(\frac{V_{u}}{V_{n}}\right) \leq 1 \quad \begin{array}{ll}
\text { Where: } & \left.\begin{array}{l}
N_{u}=\text { Applied Service Tension Load } \\
N_{n}=\text { Allowable Tension Load } \\
V_{u}
\end{array}\right) \text { Applied Service Shear Load } \\
V_{n}=\text { Allowable Shear Load }
\end{array}
$$

## Load Adjustment Factors for Spacing and Edge Distances in Concrete ${ }^{1}$

| Anchor Installed in Normal-Weight Concrete |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Anchor Dimension | Load Type | Critical Distance (Full Anchor Capacity) | Critical Load Factor | Minimum Distance (Reduced Capacity) | Minimum Load Factor |
| Spacing (s) | Tension and Shear | $s_{c r}=10 d$ | $F_{N_{s}}=F_{V_{s}}=1.0$ | $s_{\text {min }}=5 d$ | $F_{N_{S}}=F V_{V_{S}}=0.50$ |
| Edge Distance (c) | Tension | $C_{c r}=12 d$ | $F_{N_{c}}=1.0$ | $C_{\text {min }}=6 d$ | $F_{N_{c}}=0.80$ |
|  | Shear | $C_{c r}=12 \mathrm{~d}$ | $F_{V_{C}}=1.0$ | $C_{\text {min }}=6 d$ | $F V_{C}=0.50$ |

[^1]
## ORDERING INFORMATION

## Mushroom Head with No. 2 Phillips Head Screw

| Catalog Number | Anchor Size | Drill <br> Diameter | Standard <br> Box | Standard <br> Carton | Wt./I <br> 100 |
| :---: | :--- | :---: | :---: | :---: | :---: |
| 2839 | $1 / 4^{\prime \prime} \times 3 / 4^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 100 | 500 | $11 / 2$ |
| 2840 | $1 / 4^{\prime \prime} \times 1^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 100 | 500 | $13 / 4$ |
| 2842 | $1 / 4^{\prime} \times 11 / 4^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 100 | 500 | $21 / 4$ |
| 2844 | $1 / 4^{\prime \prime} \times 11 / 2^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 100 | 500 | $21 / 2$ |
| 2846 | $1 / 4^{\prime \prime} \times 22^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 100 | 500 | 3 |
| 2848 | $1 / 4^{\prime \prime} \times 21 / 4^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 100 | 500 | $31 / 2$ |
| 2850 | $1 / 4^{\prime \prime} \times 3^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 100 | 500 | $41 / 4$ |



Master Pack

| Catalog Number | Anchor Size | Drill <br> Diameter | Standard <br> Box | Standard <br> Carton | Wt./ <br> 100 |
| :---: | :--- | :---: | :---: | :---: | :---: |
| 2939 | $1 / 4^{\prime \prime} \times 3 / 4^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 1,000 | 1,000 | $11 / 2$ |
| 2940 | $1 / 4^{\prime \prime} \times 1^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 1,000 | 1,000 | $13 / 4$ |
| 2942 | $1 / 4^{\prime} \times 11 / 4^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 1,000 | 1,000 | $21 / 4$ |
| 2944 | $1 / 4^{\prime \prime} \times 11 / 2^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 1,000 | 1,000 | $21 / 2$ |
| 2946 | $1 / 4^{\prime \prime} \times 2^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 1,000 | 1,000 | 3 |
| 2948 | $1 / 4^{\prime \prime} \times 21 / 4^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 1,000 | 1,000 | $31 / 2$ |
| 2949 | $1 / 4^{\prime \prime} \times 3^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 1,000 | 1,000 | $41 / 4$ |

Mushroom Head with No. 2 Phillips Head Perma-Seal Screw

| Catalog Number | Anchor Size | Drill <br> Diameter | Standard <br> Box | Standard <br> Carton | Wt./ <br> 100 |
| :---: | :--- | :---: | :---: | :---: | :---: |
| 2817 | $1 / 4^{\prime \prime} \times 11 / 4^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 100 | 500 | $21 / 4$ |
| 2818 Master Pack | $1 / 4^{\prime \prime} \times 11 / 4^{\prime \prime}$ | $1 / 4^{\prime \prime}$ | 1,000 | 1,000 | $21 / 4$ |


[^0]:    1. Allowable load capacities listed are calculated using and applied safety factor of 4.0 . Consideration of safety factors of 20 or higher may be necessary depending upon the application such as life safety, overhead and in sustained tensile loading applications.
    2. Linear interpolation may be used to determine allowable loads for intermediate embedments and compressive strengths.
    3. Allowable load capacities are multiplied by reduction factors found in the Design Criteria section when anchor spacing or edge distances are less than critical distances.
[^1]:    1. Allowable load values found in the performance data tables are multiplied by reduction factors when anchor spacing or edge distances are less than critical distances. Linear interpolation is allowed for intermediate anchor spacing and edge distances between critical and minimum distances. When an anchor is affected by both reduced spacing and edge distance, the spacing and edge reduction factors must be combined (multiplied). Multiple reduction factors for anchor spacing and edge distance may be required depending on the anchor group configuration.
